Permit Limit Justifications

01L00155*AD

| | | | | | | | | | | | | | | | | | u | | | | | | | | | | | | | | | Ç |
|---------------|--------------------|------------------------|------------------------|-----------------------|----------------------|--------------------------------|------------------------------|------------------------------|---------------------------|-----------------|---|----------|----------|------------------------|------------------------|--------------|--------------------|------------------------|------------------------|-----------------------|----------------------|--------------------------------|------------------------------|------------------------------|-----------------|---|----------|----------|------------------------|------------------------|-----|--------------------|
| | Justificatio | NSPS | NSPS | Monitor Only | WQS-Per Guidance | WQS | NSPS | NSPS | | Monitor Only | Monitor Only | Was | WQS | NSPS | NSPS | | Justificatio | NSPS | NSPS | Monitor Only | WQS-Per Guidance | WOS | NSPS | NSPS | Monitor Only | Monitor Only | MOS | WOS | NSPS | NSPS | | Justificatio |
| | Stits | / I/bm | mg/l | | v ng/l | , l/gm | | √ l/gm | Inches | GPD | Umho/cm N | S.U. V | S.U. | ∠ I/bm | | | shun | √ l/gm | mg/l | ₩ W | v l/gm | v l/gm | √ l/gm | | GPD | Umho/cm N | S.U. V | S.U. V | Mg/l № | | | Units |
| | Tim) | 2.0 | 40 | | 1752 | 1500 | 35 | 07 | | | | 6.5 | 0.6 | 3.0 | 6.0 | | Limit | 2.0 | 4.0 | | 1752 | 1500 | 32 | 70 | | | 6.5 | 0.6 | 3.0 | 6.0 | | Limit |
| obt. Final | Rpt Code Parameter | 74013 Manganese, Total | 74013 Manganese, Total | 00940 Chloride, Total | 00945 Sulfate, (SO4) | 00515 Residue, Total Dissolved | 00530 Total Suspended Solids | 00530 Total Suspended Solids | 00045 Total Precipitation | 00056 Flow Rate | 00095 Specific Conductance at 25 Degrées C | 00400 pH | 00400 pH | 74010 Iron, Total (Fe) | 74010 Iron, Total (Fe) | onz Final | Rpt Code Parameter | 74013 Manganese, Total | 74013 Manganese, Total | 00940 Chloride, Total | 00945 Sulfate, (SO4) | 00515 Residue, Total Dissolved | 00530 Total Suspended Solids | 00530 Total Suspended Solids | 00056 Flow Rate | 00095 Specific Conductance at 25 Degrees C | 00400 pH | 00400 pH | 74010 Iron, Total (Fe) | 74010 Iron, Total (Fe) | (0) | Rpt Code Parameter |

Report Date:6/10/2011

Per l'int Justications

| Station | | | |
|---|-------|-----------|------------------|
| | | | |
| Final | | | |
| Rpt Code Parameter | E E | Units | Justification |
| 74013 Manganese, Total | 4.0 | /bm | NSPS |
| 00940 Chloride, Total | | mg/l | Monitor Only |
| 00945 Sulfate (SO4) | 1752 | l/gm | WQS-Per Guidance |
| 00515 Residue, Total Dissolved | 1500 | mg/l | WOS |
| 00530 Total Suspended Solids | 35 | ₩ Mg/l | SdSN |
| 00530 Total Suspended Solids | 70 | /bm | NSPS |
| 00056 Flow Rate | | GPD | Monitor Only |
| 00095 Specific Conductance at 25 Degrees C | | Umho/cm | Monitor Only |
| 00400 pH | 6.5 | S.U. | WQS |
| 00400 | 8.0 | S.U. | WOS. |
| 74010 Iron, Total (Fe) | 3.0 | ₩g/l | NSPS |
| 74010 Iron, Total (Fe) | 0.9 | l/gm | NSPS |
| 7,00 | | 11 | |
| | | | |
| Rpt Code Parameter | Limit | Units | Justification |
| 74013 Manganese, Total | 2.0 | l/gm | SdSN |
| 74013 Manganese, Total | 4.0 | l/gm | NSPS |
| 00940 Chloride, Total | | ₩ J/gw | Monitor Only |
| 00945 Sulfate, (SO4) | 1752 | Mg/l | WQS-Per Guidance |
| 00515 Residue, Total Dissolved | 1500 | ∥⁄gш | WQS |
| 00530 Total Suspended Solids | 35 | mg/l | NSPS |
| 00530 Total Suspended Solids | 70 | ₩ Mg/l | NSPS |
| 00056 Flow Rate | | GPD | Monitor Only |
| 00095 Specific Conductance at 25 Degrees C | | Umho/cm | Monitor Only |
| 00400 pH | 6.5 | S.U. | WOS |
| D0400 | 0.6 | S.U. | SOM |
| 74010 Iron, Total (Fe) | 3.0 | mg/l | Sasa |
| 74010 Iron, Total (Fe) | 6.0 | l/gm | SdSN |
| 100 | | | |
| Final | | | |
| Rpt Code Parameter | Limit | Units | Justification |
| 74013 Manganese, Total | 2.0 | mg/l | NSPS |
| 74013 Manganese, Total | 4.0 | mg/l | NSPS |
| 00940 Chloride, Total | | ₩g/l | Monitor Only |
| 00945 Sulfate, (SO4) | 1752 | mg/l | SOM |
| 00515 Residue, Total Dissolved | 1500 | l/6m | WOS |
| 00530 Total Suspended Solids | 35 | l/gm | NSPS |
| | | | |

Report Date:6/10/2011

WLA for North Star 1 Mine

using Short Cree near Dillonvale 03111500

7Q10

9.1 cfs

123 sq miles

1Q10

7.2

Cross Creek adjacent to Mine

7Q10

116 sq miles

equals

8.6 cfs

1Q10

116 sq miles

equals

6.8 cfs

Considering flow from site is rainfall generated and using BPJ use 10% of Average daily flow from annualized flow

with a drainage area of

156.2 flow

371900 gpd

10% of flow equals

37190 gpd

or

0.06 cfs

Upstream data to be used:

| Cross Cree RM 6.95 | Hardness | Sulfate | Chloride | TDS |
|--------------------|----------|---------|----------|-------|
| 6/23/2010 | 265 | 258 | 38.5 | 612 |
| 7/7/2010 | 467 | 326 | 47.3 | 724 |
| 7/27/2010 | 435 | 304 | 47.6 | 698 |
| 8/9/2010 | 476 | 365 | 56.6 | 770 |
| 9/13/2010 | 428 | 278 | 72.1 | 768 |
| Mean | 414.2 | 306.2 | 52.42 | 714.4 |
| Median | 435 | 304 | 47.6 | 724 |

OMZA application of TDS

Flow is less than 0.7% of streamflow

724 mg/L TDS upstream

1500 mg/L

using mass balance

117471 mg/L

this is not expected

Acute Sulfate Chloride equation

Acute sulfate=(-57.478+5.79(hardness)+54.163(chloride))*0.65

Acute sulfate=

3275.565

IMZM Sulfate=1276.7+(5.508*hardness)-(1.457*chloride)

Sulfate IMZM=

3603.327

Cross Creek Watershed 2010

Appendix Table 1. Continued.

| | | | Site Locati River Mile | Site Location: Cross Ck @ CR 26 River Mile: 9 72 Storet: COMSON | @ CR 26 | | Site Locati | on: Cross Ck | Site Location: Cross Ck @ TR 166 Dst landfills/Ust Satralloy | t landfills/Us | Satralloy |
|------------------------|----------|-----------|---------------------------|---|----------|-----------|--|--------------|--|--|-----------|
| | | | | | 100 | | | NAC NAC | 16. 0.30 SIGNET | nenine | |
| Parameter | Cnits | 6/23/2010 | 7/7/2010 | 7/27/2010 | 8/9/2010 | 9/13/2010 | 6/23/2010 | 7/7/2010 | 7/27/2010 | 8/9/2010 | 9/13/2010 |
| Acidity | mg/L | <5.0 | NA | <5.0 | <5.0 | <5.0 | <5.0 | <5.0 | <5.0 | <5.0 | <5.0 |
| Alkalinity | mg/L | 138 | AN | 163 | 151 | 152 | 131 | 144 | 147 | 153 | 135 |
| Aluminum | ng/L | <200 | <200 | <200 | <200 | <200 | 314 | <200 | 464 | 333 | 222 |
| Ammonia | mg/L | <0.050 | AN | <0.050 | <0.050 | <0.050 | <0.050 | <0.050 | <0.050 | <0.050 | <0.050 |
| Arsenic | ug/L | <2.0 | <2.0 | <2.0 | <2.0 | <2.0 | <2.0 | <2.0 | <2.0 | <2.0 | <2.0 |
| Sarium | ng/L | 54 | 63 | 61 | 09 | 56 | 53 | 61 | 62 | 58 | 55 |
| Cadmium | ng/L | <0.20 | <0.20 | <0.20 | <0.20 | <0.20 | <0.20 | <0.20 | <0.20 | <0.20 | <0.20 |
| Calcium | mg/L | 117 | 128 | 127 | 123 | 117 | 106 | 126 | 118 | 128 | 117 |
| Chloride | mg/L | 31.2 | 33.1 | 37.5 | 44.6 | 45.6 | 38.5 | 47.3 | 47.6 | 56.6 | 72.1 |
| Chromium | ug/L | <2.0 | <2.0 | <2.0 | <2.0 | <2.0 | <2.0 | <2.0 | <2.0 | <2.0 | <2.0 |
| COD | T/6w | <20 | <20 | <20 | <20 | <20 | <20 | <20 | <20 | <20 | <20 |
| Conductivity | nmhos/cm | 864 | NA | 1040 | 1050 | 1050 | 855 | 974 | 974 | 1100 | 1070 |
| Copper | ng/L | <2.0 | <2.0 | <2.0 | <2.0 | <2.0 | <2.0 | <2.0 | 2.7 | 2.2 | 2 |
| Hardness, Total | mg/L | 27.7 | 488 | 482 | 468 | 449 | 265 | 467 | 435 | 476 | 428 |
| Iron | ng/L | 204 | 129 | 158 | 89 | 66 | 673 | 266 | 936 | 686 | 408 |
| Lead | ng/L | <2.0 | <2.0 | <2.0 | <2.0 | <2.0 | <2.0 | <2.0 | <2.0 | <2.0 | <2.0 |
| Magnesium | mg/L | 32 | 41 | 40 | 39 | 38 | 30 | 37 | 34 | 38 | 33 |
| Manganese | ng/L | 40 | 43 | 49 | 47 | 45 | 28 | 62 | 155 | 89 | 102 |
| Nickel | ng/L | 2.8 | 2.7 | 2.7 | 2.1 | 2 | 3.5 | 3.2 | 4 | 3.5 | 3.9 |
| Nitrate+nitrite | mg/L | 0.22 | Ā | 0.14 | <0.10 | <0.10 | 0.27 | 0.16 | 0.43 | <0.10 | 1.55 |
| Nitrite | mg/L | <0.020 | <0.020 | <0.020 | <0.020 | <0.020 | <0.020 | <0.020 | <0.020 | <0.020 | <0.020 |
| Potassium | mg/L | က | က | 4 | 4 | 4 | m | 4 | 4 | 4 | 5 |
| Selenium | ng/L | <2.0 | <2.0 | <2.0 | <2.0 | <2.0 | <2.0 | <2.0 | <2.0 | <2.0 | <2.0 |
| Sodium | mg/L | 27. | 32 | 42 | 14 | 41 | 27 | 33 | 40 | 47 | 49 |
| Strontium | ng/L | 526 | 653 | 299 | 613 | 607 | 472 | 584 | 543 | 589 | 508 |
| Sulfate | mg/L | 276 | 355 | 359 | 373. | 323 | 258 | 326 | 304 | 365 | 278 |
| TKN | mg/L | <0.20 | ΑN | 0.35 | 0.34 | 0.39 | 0.23 | 0.39 | 0.28 | 0.41 | 0.59 |
| Total Dissolved Solids | mg/L | 909 | 720 | 732 | 756 | 782 | 612 | 724 | 869 | 770 | 768 |
| Total Phosphorus | mg/L | 0.01 | Ϋ́ | 0.015 | 0.015 | <0.010 | 0.048 | 0.043 | 0.079 | 0.059 | 0.141 |
| Total Suspended Solids | mg/L | \$ | 9 | <5 | <5 | 2 | 20 | 6 | 41 | 17 | 10 |
| Zinc | ng/L | ×10 | <10 | <10 | <10 | <10 | <10 | <10 | <10 | <10 | <10 |
| Field Measurements | | | | | | | | | | MONORIO E FRANCE ESPECIAL ESPE | |
| Temperature | ပ္စ | 25.11 | 27.18 | 25.17 | 26.68 | 20.94 | 25.09 | 25.4 | 26.19 | 24.1 | 18.89 |
| Conductivity | mp/soumn | 853.9 | 999.2 | 1015.1 | 1035.8 | | 722.7 | 993.5 | 961.5 | 1072.5 | 1046.5 |
| Dissolved Oxygen | mg/L | 9.68 | 8.99 | 9.2 | 9.31 | 9.72 | 7.46 | 9.19 | 7.48 | 10.2 | 11.08 |
| D.O. Saturation | % | 117.6 | 113.5 | 112 | 116.5 | 109.2 | 9.06 | 112.3 | 92.8 | 121.7 | 119.5 |
| Ha | S.U. | 8.17 | 8.14 | 7.84 | 8.34 | 8.11 | 8.43 | 8:31 | 8.41 | 8.26 | 8.29 |
| | | | | | | - Aire | Personal property of the Personal Perso | | | THE ACTION OF THE PROPERTY OF | |

Permitting of Dissolved Inorganics for Coal Individual Permits

This also has info on metals and mercury

Introduction

As soon as we receive a renewal application ask for more effluent data for hardness, chloride, etc.

To provide some guidance through the changes related to TDS, we are providing district staff with rule citations and methods for developing WQ-based effluent limits and other permit conditions related to dissolved solids and its constituent ions.

The toxicity of total dissolved solids is related to both the toxic effect of specific ions and the total additive effect of those ions. An example of the first effect is that effluents that have the same overall TDS concentration may have different toxicities based on the anions present discharges that have higher sulfate concentrations are more toxic than discharges where chloride is the primary anion. The toxicity of TDS in an effluent is also related to the concentration of bicarbonate ions (water hardness). Increases in w ater hardness mitigate toxic effects between hardness concentrations of 100 mg/l to 500 mg/l. Hardness concentrations above 500 mg/l may add to toxicity by adding to the total ion concentration in the water.

To account for the different toxicities of different ion mixes, we have developed formula to calculate water quality criteria for sulfate and chloride based on hardness. Usually limits are set for the primary anion based on receiving water hardness, and an assumed concentration of the other ion (Sulfate, being the primary anion in coal process wastewaters, has criteria that depend on hardness and chloride concentrations in the stream).

We must still do a WQBEL for chronic TDS

In permits where sulfate is the primary toxic component of TDS, a maximum sulfate WQBEL is used instead of a maximum TDS WQBEL.

If chloride is the primary toxic component I think we'd also do a WQBEL for chloride

Here is the formula:

Acute sulfate criterion = [-57.478+5.79(hardness) + 54.163(chloride)]*0.65. The maximum hardness used in this formula is 500 mg/l. If the receiving water hardness is >500 mg/l, use 500 ma/l in the criterion formula.

There is also a formula for chloride it we to use

IMZM criterion = 1276.7 mg/l + (5.508*hardness) - (1.457*chloride)

Unless the stream provides significant dilution, the acute criterion will be more restrictive than IMZM

Note that, unlike other aquatic life criteria, the IMZM for sulfate is less than two times the OMZM Some mines will have new discharges that will have the same or very similar quality as the current discharges at

criterion.

a mine or discharges from other nearby surface mines they operate. In that case we should ask for the form 2C and 2D for the new outfalls based on sampling of the existing discharges. The form 2D provides some **Applications** information the 2C doesn't. We also need drainage areas for each outfall to calc. an ADF.

We will be receiving either Application Form 2C or 2D for each site. Form 2C (existing sources and those new sources that can project data from existing facilities) will have data for sulfate from Part V, B. of the application. Form 2D (new facilities) will require an estimate of sulfate concentrations.

With either application, we should require the facility to submit effluent data for TDS and chloride. If the facility has downstream data for hardness and chloride on the receiving water, they should submit that, too. The downstream data is used to calculate the WQS for sulfate.

I assume this means downstream data if the mine already has discharges to the stream. If it's a brand new discharge from a new mine there is no upstream of downstream yet unless the site has already been impacted by mining.

ODNR may have WQ data and discharge data for mines and that they reportedly require stream sampling results to be submitted with the mine application to ODNR. This may be a good source of information.

Use this data if calc. a chloride limit if chloride is the primary pollutant Any upstream data for sulfate, TDS or metals should also be required if available. In our modeling rules, median or mean concentrations are used as back ground if data are available from the receiving water or a representative local stream. If no background data are available, we would use the 25th percentile of a reference data set, such as the Western Allegheny Plateau (WAP) Ecoregion data shown below (again, specified in our modeling rules):

| 2-14-14-14-14-14-14-14-14-14-14-14-14-14- | | Reference Site | S | Mir | ne-affected S | tes |
|---|----------|----------------|----------|----------|---------------|----------|
| Percentile | Hardness | → Sulfate | Chloride | Hardness | Sulfate | Chloride |
| 10 | 116 | 25 | 12 | 120 | 38 | 8 |
| 25 | 145 | 33 | 18 | 196 | 72 | 13 |
| 50 | 208 | 53 | 27 | 281 | 153 | 24 |
| 75 | 258 | 142 | 40 | 417 | 360 | 44 |
| 95 | 419 | 259 | 86 | 948 | 945 | 126 |

The data for mine-affected sites should be used if there has been any mining in the HUC-12 watershed. This should cover most of the waterbodies in coal-bearing areas of the WAP. For watersheds that have not had mining discharges or surface effects in the past, the ecoregion reference site data should be used.

See my recent email about HUC 12 Watersheds.

The values in this table can be presented as default values to be used in the absence of local data. If the applicant wishes to collect local data, this data may guide that decision.

Discharge Limits

Limits for TDS are calculated in the same way as other WQBELs for TDS. You can use either the WLA spreadsheet, or calculate the limits by hand. The inputs for this allocation are:

WQS = 1500 mg/l

Could ask Kelly to help with these low flows like /e've done in the past.

If discharge is dependent on precipitation, the effluent flow should be calc. as we've done in the past using the drainage area and annual average rainfall divided by 365 and assuming 80% runoff using the Excel spreadsheet.

Annual 7Q10 flow – from USGS low-flow book or other reference (another discharger's WLA, for example). Remember to incorporate the % of effluent flow used in the allocation (the spreadsheet does this automatically) – [OAC 3745-2-05(A)(2)].

Effluent flow – "a reasonable measure of average flow" [OAC 3745-2-05(A)(4)(b)]. We normally use an upper bound of the average flow. Measures of this flow might be either the maximum 30-day average flow from the application, the 95th percentile of reported monthly average flows, or for new discharges, a design average flow.

Upstream concentrations of pollutants – Combine any upstream data reported by the applicant with any applicable data available from OEPA surveys or compliance samplings. The upstream concentration for the WLA is the 50th percentile if N≥10, or the mean if N is less than 10 samples. [OAC 3745-2-05(A)(3)]. If no representative data exists for a particular receiving water use data from: (1) an adjacent stream; or (2) background water quality data for the ecoregion or from the background water quality report. If data from (2) is used, the background concentration will be the 25th percentile of the data. [OAC 3745-2-04(E)(1)(b)].

Limits for sulfate need to be calculated by hand at the moment; criteria are not in the WLA spreadsheet yet. The downstream WQS are calculated from the downstream data. Measures

of hardness and chloride need to be calculated using the 50th percentile for N≥10, or the mean if N is less than 10 samples.[OAC 3745-2-04(E)(1) - This rule addresses only hardness, but it is reasonable to apply it to chloride as well]. If no representative data exists for a particular receiving water use 25th percentile data from the WAP Ecoregion in the table above.

Use effluent hardness and chloride if the discharge makes up most all flow in the stream

If the discharge

there is dilution.

there may be an

opportunity to store the runoff

or other mine discharges and

release when

stream flows

are adequate.

storage and stream flow

measurement and appropriate

permit

monitoring

requirements and conditions.

This will require

ma

sta

ા meet

ds and

Effluent data may be used in this calculation only if the pond or other treatment system represents the headwater of the stream.

Effluent flows for sulfate and metals should be the same as those used in the TDS WLA.

Critical flows should be used in the WLA calculation, as provided in our modeling rules, as a default. For sulfate maximum criteria, use the 1Q10 flow. For metals and other pollutants, the

critical flows are:

Average aquatic life: 7Q10 (except ammonia-N: 30Q10)

Maximum aquatic life: 1Q10 (except ammonia-N: 7Q10)

Human Health and Agricultural Water Supply: Harmonic mean

You can "dilute" to meet WQ based effluent limits. After meeting tech, based limits, the discharge could combine with site runoff in another settling pond (including sanitary) so WQ based limits are met at end of pipe before the stream.

These outfalls may not discharge at critical flows. If the discharge does not occur to the head of a stream, WLAs and permit conditions can be structured to reflect alternate dilutions. In this case, a minimum stream flow needs to be defined, and the permit written to prohibit discharges at flows less than the defined stream flow (similar to permit conditions for controlled lagoon types of sewage treatment plants). All WLAs would be calculated using this alternate dilution; all reasonable potential determinations and permit conditions would be based on this alternate dilution unless a critical flow WLA yields a higher WLA.

Note that the mixing zone ban applies to allocations for mercury and other bioaccumulative chemicals of concern (BCCs). WLAs and any needed limits for mercury must be based on WQS at the discharge point.

Monitoring

Process discharges should be monitored for other components of TDS at a quarterly frequency. These include sodium, calcium, magnesium, hardness and chloride. For existing discharges, or new dischargers using Form 2C, the permit should also contain monitoring requirements for selenium, low-level mercury and any other metals that are listed in Group 4 or Group 5 of the WLA hazard assessment. For new dischargers using Form 2D, the permit should include monitoring for all priority pollutant metals at least annually (selenium and mercury should be at least quarterly).

From the WLA spreadsheet.

We may want to also get some downstream hardness and chloride monitoring in the permit to help in future permit development.



Streamstats Ungaged Site Report

Date: Fri May 27 2011 12:18:45 Mountain Daylight Time Site Location: Ohio
NAD27 Latitude: 40.3044 (40 18 16)
NAD27 Longitude: -80.6772 (-80 40 38)
NAD83 Latitude: 40.3045 (40 18 16)
NAD83 Latitude: 40.3045 (40 18 16) NAD83 Longitude: -80.6770 (-80 40 37) Drainage Area: 116 mi2

| 100% Peak Flow Full Model (116 mi2) | | | |
|--|-------|----------------|-------------------|
| Parameter | Value | Regression Equ | ation Valid Range |
| randes | | Min | Max |
| Drainage Area (square miles) | 116 | 0.01 | 7422 |
| Ohio Region C Indicator 1 if in C else 0 (dimensionless) | 0 | 0 | 1 |
| Ohio Region A Indicator 1 if in A else 0 (dimensionless) | 0 | 0 | 1 |
| Stream Slope 10 and 85 Longest Flow Path (feet per ml) | 14.9 | 1.53 | 674 |
| Percent Storage from NLCD (percent) | 1.97 | 0 | 25.8 |

| Y coordinate (latitude) of the centroid in de- | cimal degre | ees=40.3624 | |
|--|-------------|---------------------|----------------|
| 100% Low Flow Lattitude LE 41.2 (116 mi2 |) | | |
| Parameter | Value | Regression Equation | on Valid Range |
| raiameter | | Min | Max |
| Drainage Area (square miles) | 116 | 0.12 | 7422 |
| Percent Forest (percent) | 59.2 | 0 | 99.1 |
| Percent Storage from NLCD (percent) | 1.97 | 0 | 19 |
| Mean Annual Precipitation (inches) | 39.4 | 34 | 43.7 |
| Streamflow Variability Index (dimensionless) | 0.47 | 0.25 | 1.13 |
| Latitude of Basin Centroid (decimal degrees) | 40.3625 | 38.68 | 41.3 |
| Longitude of Basin Centroid (decimal degrees) | 80.8131 | 80.53 | 84.0 |

| Peak Fl | ows Strea | mflow Statistics | | | |
|-----------|---------------------------|----------------------------|-----------------|----------------|------------------|
| | | | Equivalent | 90-Percent Pre | diction Interval |
| Statistic | Flow (ft ³ /s) | Prediction Error (percent) | years of record | Minimum | Maximum |
| PK2 | 2350 | 37 | 2.1 | 1250 | 4410 |
| PK5 | 3520 | 35 | 3.3 | 1940 | 6390 |
| PK10 | 4320 | 34 | 4.4 | 2380 | 7830 |
| PK25 | 5250 | 35 | 5.9 | 2840 | 9700 |
| PK50 | 5920 | 37 | 6.8 | 3140 | 11200 |
| PK100 | 6590 | 38 | 7.5 | 3410 | 12800 |
| PK500 | 8020 | 42 | 8.6 | 3870 | 16600 |

| | | | Equivalent | 90-Percent Pre | diction Interva |
|-----------|---------------------------|----------------------------|-----------------|----------------|-----------------|
| Statistic | Flow (ft ³ /s) | Prediction Error (percent) | years of record | Minimum | Maximum |
| Q1 | 195 | 17 | | | |
| Q2 | 214 | 12 | | | |
| Q3 | 257 | 14 | | | |
| Q4 | 220 | 11 | | | |
| Q5 | 141 | 20 | | | - |
| | 95.9 | | | | |

Streamflow Statistics Report

| Q6 | | 27 | | |
|-------|------|----|--|--|
| Q7 | 59.6 | 28 | | |
| Q8 | 50 | 37 | | |
| Q9 | 37.9 | 44 | | |
| QA | 135 | 11 | | |
| Q10 | 31.5 | 51 | | |
| Q11 | 67.7 | 38 | | |
| Q12 | 137 | 22 | | |
| QAH | 29.9 | 66 | | |
| FPS25 | 24.4 | 29 | | |
| FPS50 | 70.9 | 40 | | |
| FPS75 | 157 | 48 | | |



Ohio StreamStats

Flow Estimates Based on Flows at Nearby Streamgaging Stations

Date: Fri May 27 2011 12:21:46 Mountain Daylight Time

NAD27 Latitude: 40.3044 (40 18 16) NAD27 Longitude: -80.6772 (-80 40 38) NAD83 Latitude: 40.3045 (40 18 16) NAD83 Longitude: -80.6770 (-80 40 37)

ReachCode: 05030101000557

Measure: 92.90

User-Selected Site Watershed Area, in square miles: 116

Use Regulated Station: No

Warning:

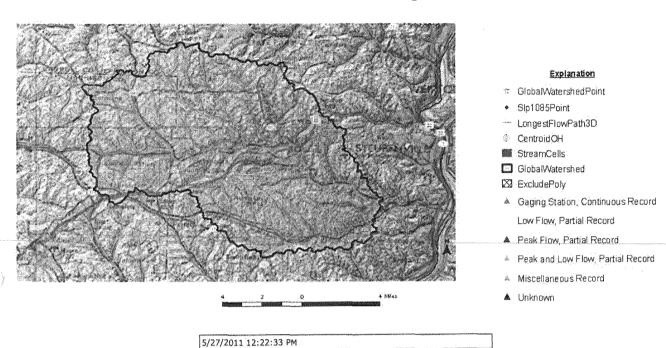
No upstream or downstream gaging station has a drainage area that is within 50 percent of the drainage area for the selected ungaged site, thus no further computations can be completed.

Upstream Gage
No records found.

Downstream Gage
No records found.



StreamStats Print Page



Name: North Star 1 Mine

| | Drainage Area Acres | Average Daily Flow from Runoff * (gpd) | Additional Flow , e.g. Process Wastewater (gpd) | Total Flow gpd (Column C + D) |
|--------------|------------------------|--|---|--------------------------------|
| Outfall: 001 | 30.1 16.1 | 71657 38328 | 0 | 71700 38300 |
| Outfall: 002 | | 11665 | 0 | 11700 |
| Outfall: 003 | 4.9 33.9 | 80704 | 0 | 80700 |
| Outfall: 004 | | 52612 | 0 | 52600 |
| Outfall: 005 | 22.1 | | | 19500 |
| Outfall: 006 | 8.2 | 19521 | 0 | |
| Outfall: 007 | 40.9 | 97368 | 0 | 97400 |
| | | * ((Acres*40/12*3258 | 51*0.8)/365) | |

 $^{0.8 = \}text{runoff coef.}$

A. Pennyton

JEFFERSON

PUBLIC NOTICE

The following applications and/or verified complaints were received, and the following draft, proposed and final actions were issued, by the Ohio Environmental Protection Agency (OEPA) last week. "Actions" include the adoption, modification, or repeal of orders (other than emergency orders); the issuance, denial, modification or revocation of licenses, permits, leases, variances, or certificates; and the approval or disapproval of plans and specifications. "Draft actions" are written statements of the Director of Environmental Protection's (Director's) intent with respect to the issuance, denial, etc. of a permit, license, order, etc. Interested persons may submit written comments or request a public meeting regarding draft actions. Comments or public meeting requests must be submitted within 30 days of notice of the draft action. "Proposed actions" are written statements of the Director's intent with respect to the issuance, denial, modification, revocation, or renewal of a permit, license or variance. Written comments and requests for a public meeting regarding a proposed action may be submitted within 30 days of notice of the proposed action. An adjudication hearing may be held on a proposed action if a hearing request or objection is received by the OEPA within 30 days of issuance of the proposed action. Written comments, requests for public meetings and adjudication hearing requests must be sent to: Hearing Clerk, Ohio Environmental Protection Agency, P.O. Box 1049, Columbus, Ohio 43216-1049 (Telephone: 614-644-2129). "Final actions" are actions of the Director which are effective upon issuance or a stated effective date. Pursuant to Ohio Revised Code Section 3745.04, a final action may be appealed to the Environmental Review Appeals Commission (ERAC) by a person who was a party to a proceeding before the Director by filing an appeal within 30 days of notice of the final action. Pursuant to Ohio Revised Code Section 3745.07, a final action issuing, denying, modifying, revoking or renewing a permit, license or variance which is not preceded by a proposed action, may be appealed to the ERAC by filing an appeal within 30 days of the issuance of the final action. ERAC appeals accompanied by a \$70.00 filing fee which the Commission in its discretion may reduce if by affidavit the appellant demonstrates that payment of the full amount of the fee would cause extreme hardship, must be filed with: Environmental Review Appeals Commission, 309 South Fourth Street, Room 222, Columbus, Ohio 43215. A copy of the appeal must be served on the Director within 3 days after filing the appeal with ERAC.

APPLICATION FOR ANTIDEGRADATION PROJECT

OHIO AMERICAN ENERGY, INC. - NORTH STAR 1 MINE 34 KELLEY WAY

BRILLIANT, OH 43913 OH ACTION DATE: 04/19/2011

RECEIVING WATERS: MCINTYRE CREEK AND CROSS CREEK

FACILITY DESCRIPTION: WASTEWATER IDENTIFICATION NO. : 01L00155

ANTIDEGRADATION PROJECT AS DEFINED BY OAC 3745-1-05 - AN EXCLUSION OR WAIVER IS NOT APPLICABLE. REQUESTS TO BE ON THE INTERESTED PARTIES MAILING LIST SHOULD BE SUBMITTED WITHIN 30 DAYS TO OHIO EPA-DIVISION OF SURFACE WATER, ATTENTION: PERMITS PROCESSING UNIT, 50 WEST TOWN STREET, P.O. BOX 1049, COLUMBUS, OHIO 43216-1049.

April 19, 2011

Ohio American Energy: Antidegradation

resulting from the project or approval of the application. The exclusions refer to the level of the requested discharge in relation to what the stream or receiving water can handle safely (e.g. application proposed to discharge at less then ten percent of what the stream can accept) or that an environmental benefit will result from the proposed activity (e.g. cleanup of contaminated ground water, providing sewage services to homes with unsanitary conditions. etc.).

The exclusions are outlined by the rules and Ohio EPA makes the determination if a project and/or application meets the appropriate conditions. If a project is determined to meet one of these exclusions, the application and review process is somewhat streamlined since a detailed analysis for environmental, human health and water resource protection is not warranted.

Will the WQS be lowered? What is the risk to the environment and public health? What is meant by a lowering of water quality?

Any project that is subject to the antidegradation rule will result in a "lowering of water quality" by definition. However, this does not mean that the utilization of that water body for recreational purposes, water consumption or other direct or indirect utilization will be harmed or that the aquatic life and fish communities present in EPA in writing. Once this initial that water body are impacted or harmed in any way. In simple terms, a "lowering of water quality" simply means that the existing instream conditions may be modified by the proposal-it will be a different environment within the water that will still be protective of all uses for that water

body. Though there will be this "lowering of water quality," at no time will any discharge be able to exceed the values derived in Ohio water quality standards that were developed to protect all ultimate uses of a water body.

How can I learn more about the project under consideration?

All discharge or construction permit applications are initially submitted to the district office responsible for that geographic area. The district offices are responsible for coordinating the review and/or evaluation of these applications. Copies of all applications including detailed design drawings and any associated correspondence with the applicant can be viewed at the appropriate district office.

What is the antidegradation review schedule? How can I comment on this proposal?

Initially, once the application is received and notice issued there is a 30 day comment period from the date of this notice/fact sheet-this date is documented on this fact sheet. During this period, interested parties can request to be kept informed of the project by being placed on the mailing list for the project and may also request a hearing on the application or proposal if one has not already been scheduled. Such requests need to be forwarded to the Ohio comment period is over, a draft/proposed permit action may be taken recommending either approval or denial of the application. This then would have an additional comment period of at least 30 days before a final action can be taken on the application.

For More Information

To be placed on the interested parties mailing list, request a public hearing or request additional information relative to this project you should contact Ohio EPA in writing at:

Ohio EPA Division of Surface Water 50 West. Town Street, Suite 700 P.O. Box 1049 Columbus, OH 43216-1049.

Also, additional information can be obtained by contacting the Division of Surface Water staff at the appropriate district office.

Ohio EPA District Offices

Ohio EPA-Southeast District Office 2195 Front Street Logan, Ohio 43138 (740) 385-8501

Ohio EPA-Southwest District Office 401 East Fifth Street Dayton, Ohio 45402-2911 (937) 285-6357

Ohio EPA-Northwest District Office 347 N. Dunbridge Road Bowling Green, Ohio 43402 (419) 352-8461

Ohio EPA-Northeast District Office 2110 East Aurora Road Twinsburg, Ohio 44087 (330) 963-1200

Ohio EPA-Central District Office 50 West Town Street, Suite 700 Columbus, Ohio 43215 (614) 728-3778

INTER-OFFICE COMMUNICATION

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